Model Predictive Control based Driver Support for Docking of Articulated Vehicles at Logistics Areas

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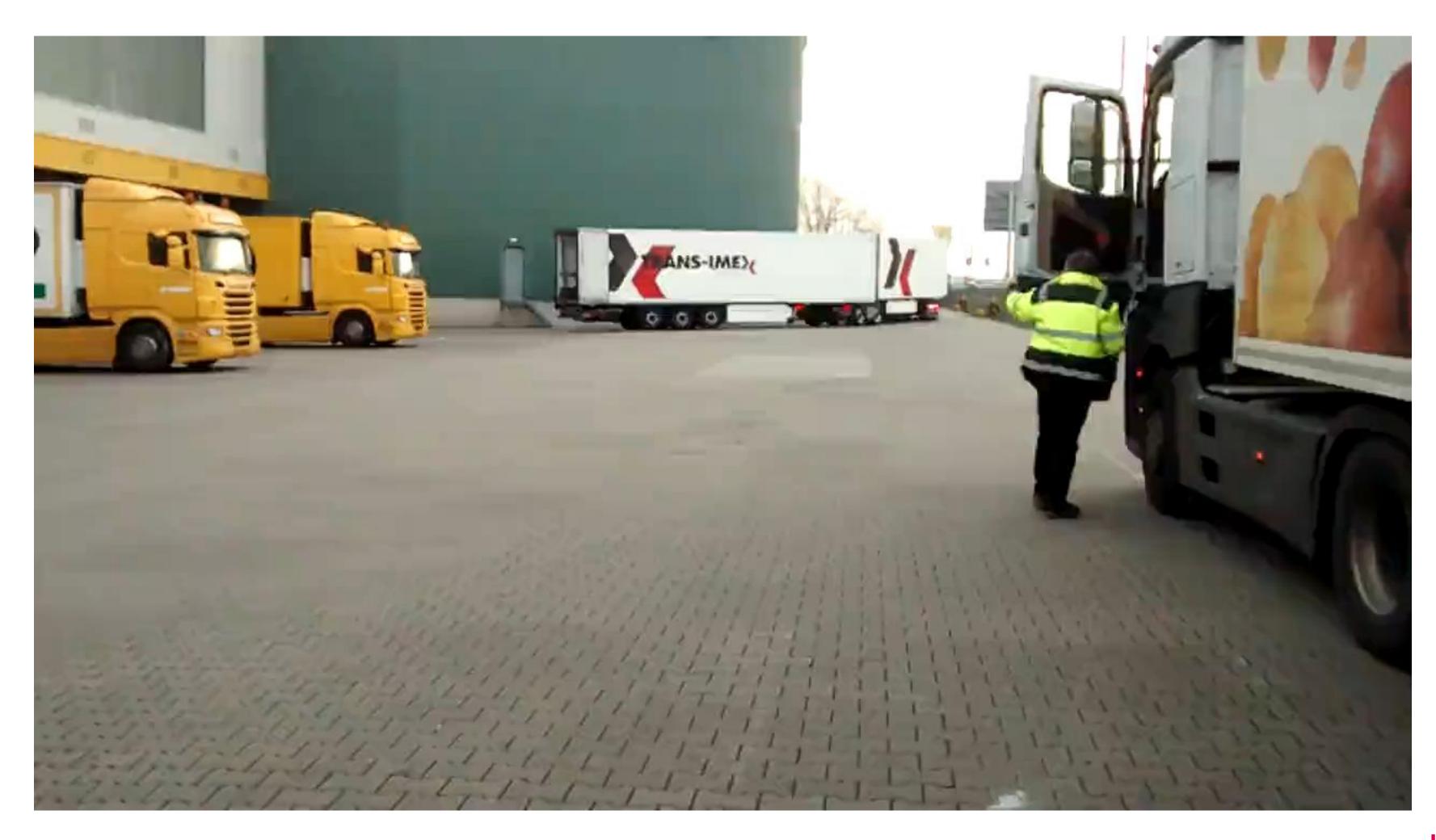
Content

- Introduction & Context
- Controller Requirements and Interfaces
- Controller Structure
- Controller Implementation and Verification
- Conclusions and Research Outlook





AVEC'22 Current Situation at many distribution centres (4 x Faster)



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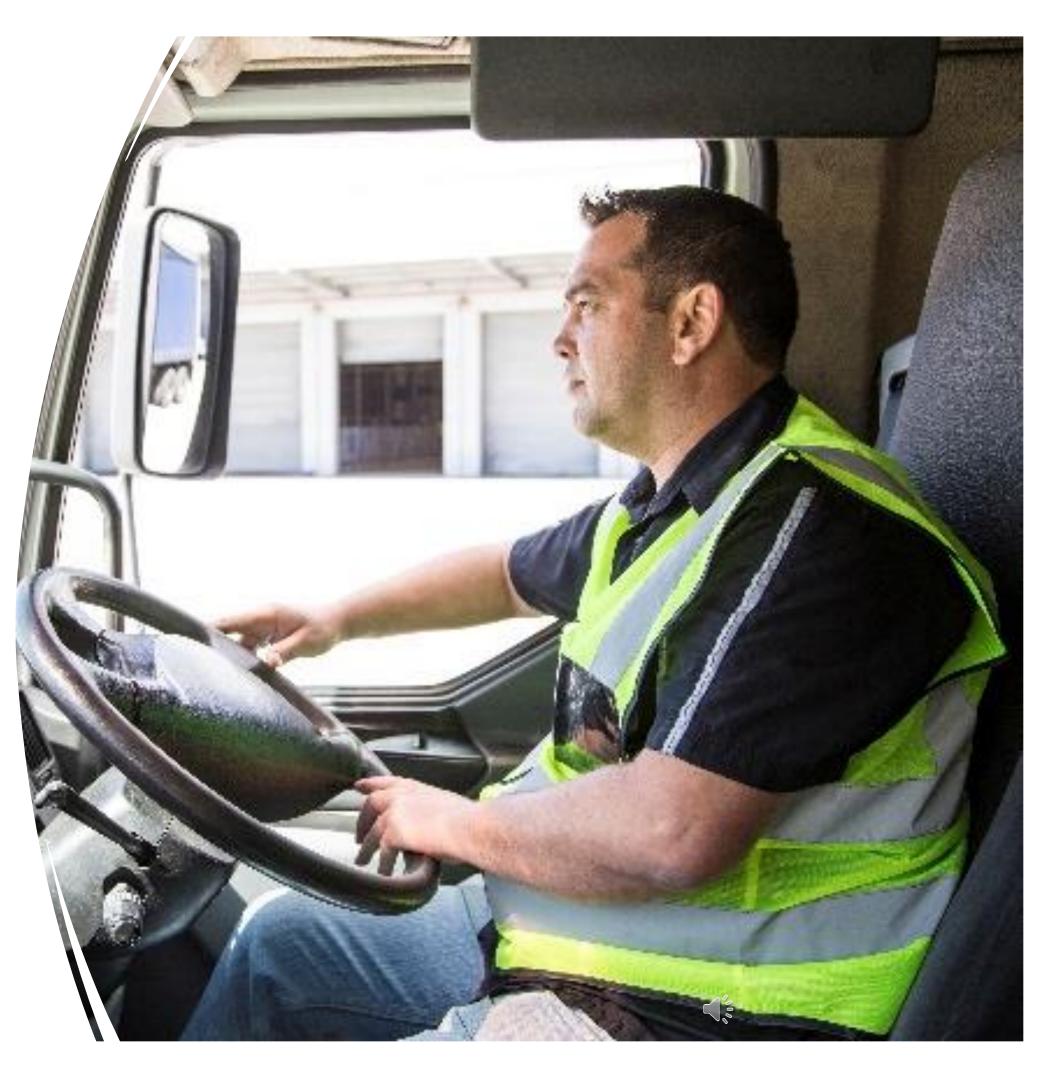




Driver Challenges

- Limited field of view
- Controlling naturally unstable system
- Limited manoeuvrability space
- Keep the safety on first place under the high pressure of productivity





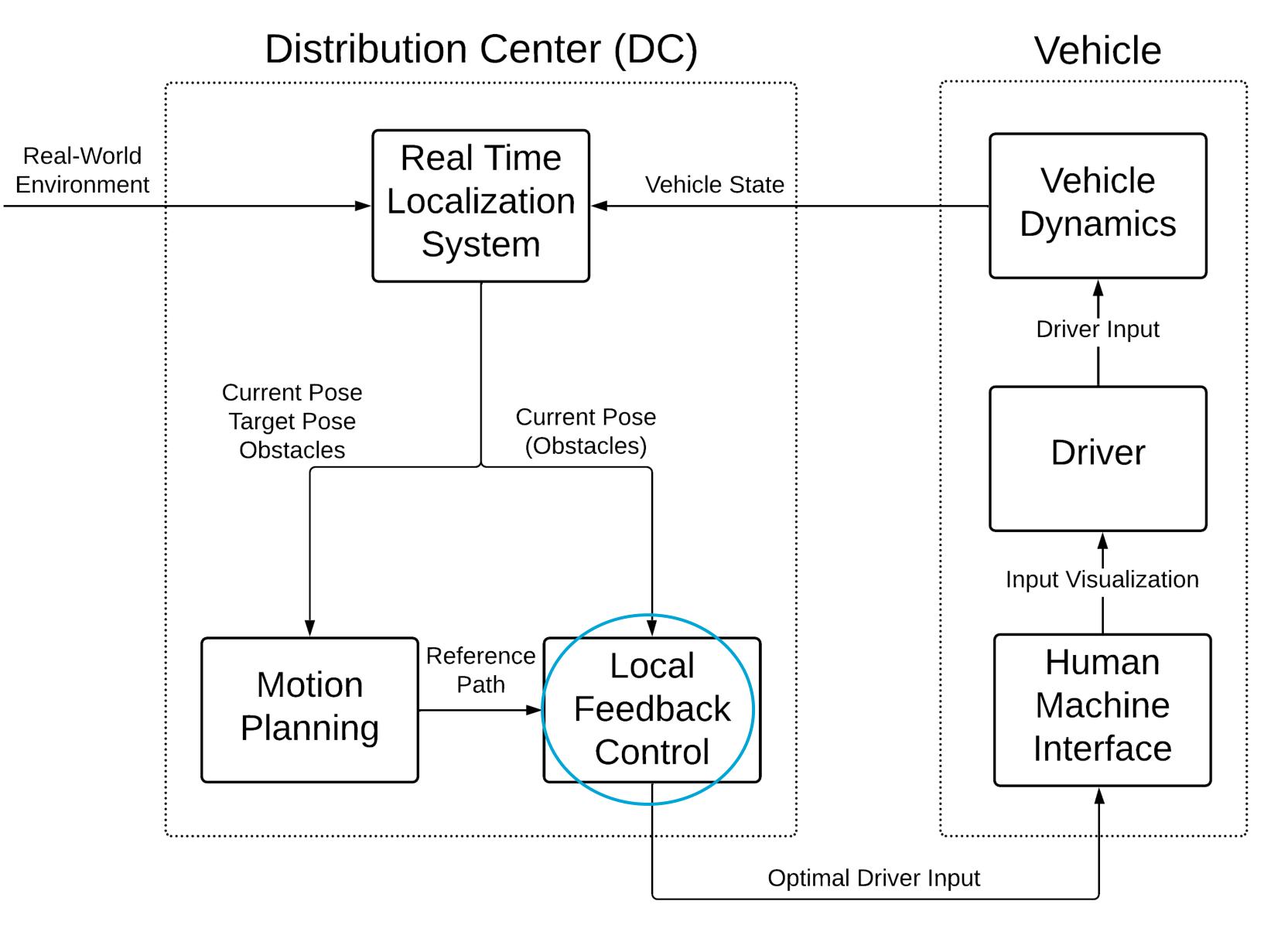








System Architecture





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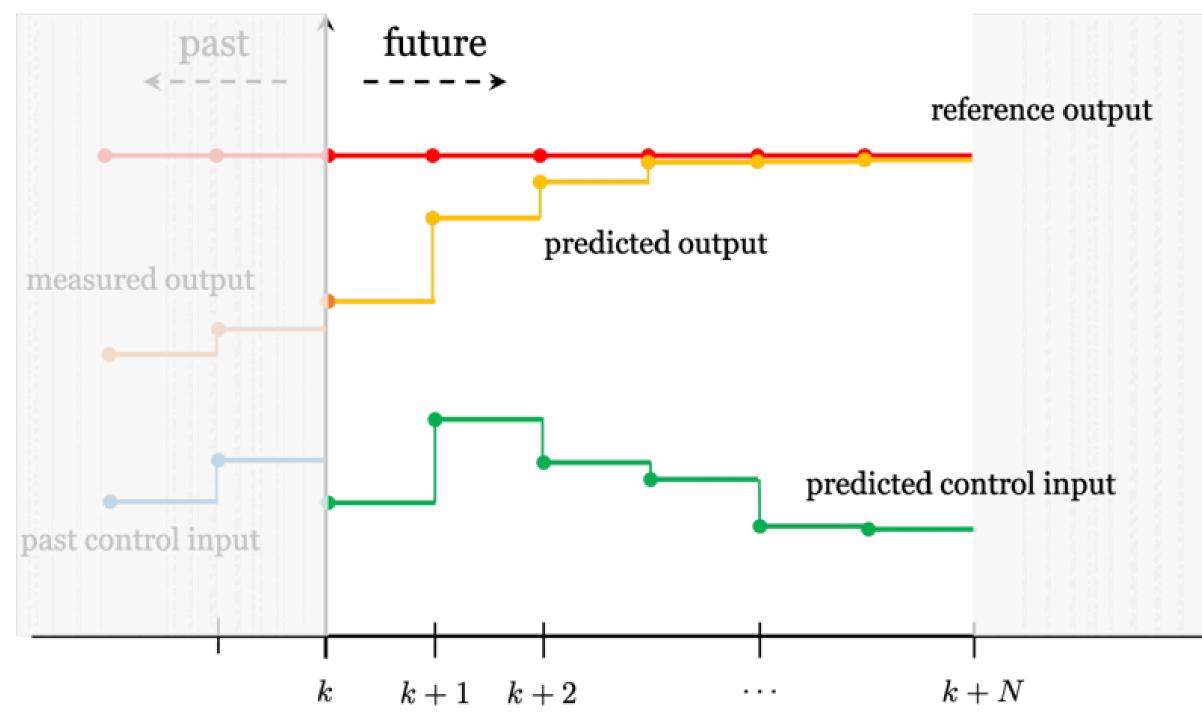
Path Tracking Controller requirements

- •Ability to incorporate driver (model) behaviour as imperfect actuator
- Robustness against the disturbances and constraints
- •Bi-directional functionality
- •Choice: Receding Horizon Control (RHC), also known as Model Predictive Control (MPC)

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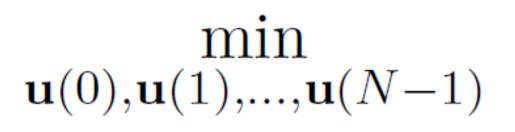




Optimization Problem



System dynamicsConstraints

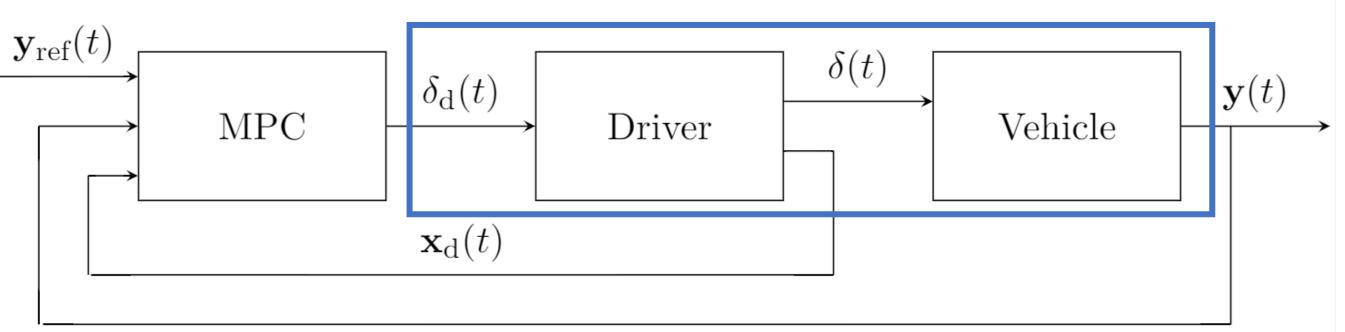


s.t.

•

N $\sum J(\mathbf{x}(k), \mathbf{u})$ k=0 $\mathbf{x}(0)$ $= \mathbf{x}_{\text{init}},$ $\mathbf{x}(k+1) = f$ $g(\mathbf{x}(k), \mathbf{u}(k))$ $h(\mathbf{x}(k), \mathbf{u}(k))$





$$\mathbf{u}(k)),$$

$$\begin{aligned} \forall k \in \{0, 1, \dots, N-1\}, \\ 0 = 0 \\ 0 \leq 0 \end{aligned} \quad \forall k \in \{0, 1, \dots, N\}, \\ \forall k \in \{0, 1, \dots, N\}. \end{aligned}$$

Vehicle Behaviour Representation

 $\dot{\mathbf{x}}(t) =$

- •Kinematic model of single articulated vehicle
- •Geometry based on envelope of common dimensions of EU Tractor-Semitrailer
- •Assumption no tyre slip and inertial effects
- •Validity only at low speeds



(x_{0f}, y_{0f}) $v_0 \left(\cos \gamma_1 \cos \theta_1 - \frac{L_{0b}}{L_{0f}} \cos \theta_1 \tan \delta \right)$ $\begin{bmatrix} v_0 \left(\cos \gamma_1 \sin \theta_1 - \frac{L_{0b}}{L_{0f}} \sin \gamma_1 \sin \theta_1 \tan \delta \right) \\ v_0 \left(\frac{1}{L_{1f}} \sin \gamma_1 + \frac{L_{0b}}{L_{0f}L_{1f}} \cos \gamma_1 \tan \delta \right) \\ v_0 \left(\frac{1}{L_{0f}} \tan \delta - \frac{1}{L_{1f}} \sin \gamma_1 - \frac{L_{0b}}{L_{0f}L_{1f}} \cos \gamma_1 \tan \delta \right) \end{bmatrix}$ θ_0 L_{1f} (x_{1f}, y_{1f}) $y_{\mathcal{B}_0}$ (x_0, y_0) L_{0b} $y_{\mathcal{B}_1}$ (x_1, y_1) HAN_UNIVERSITY **OF APPLIED SCIENCES**





Driver Behaviour Representation

- McRuerer model
- •2nd order LTI
- Driver delay compensation

$$H(s) = K \frac{(T_L s + 1)}{(T_l s + 1)(T_N s + 1)} e^{-\tau s}$$

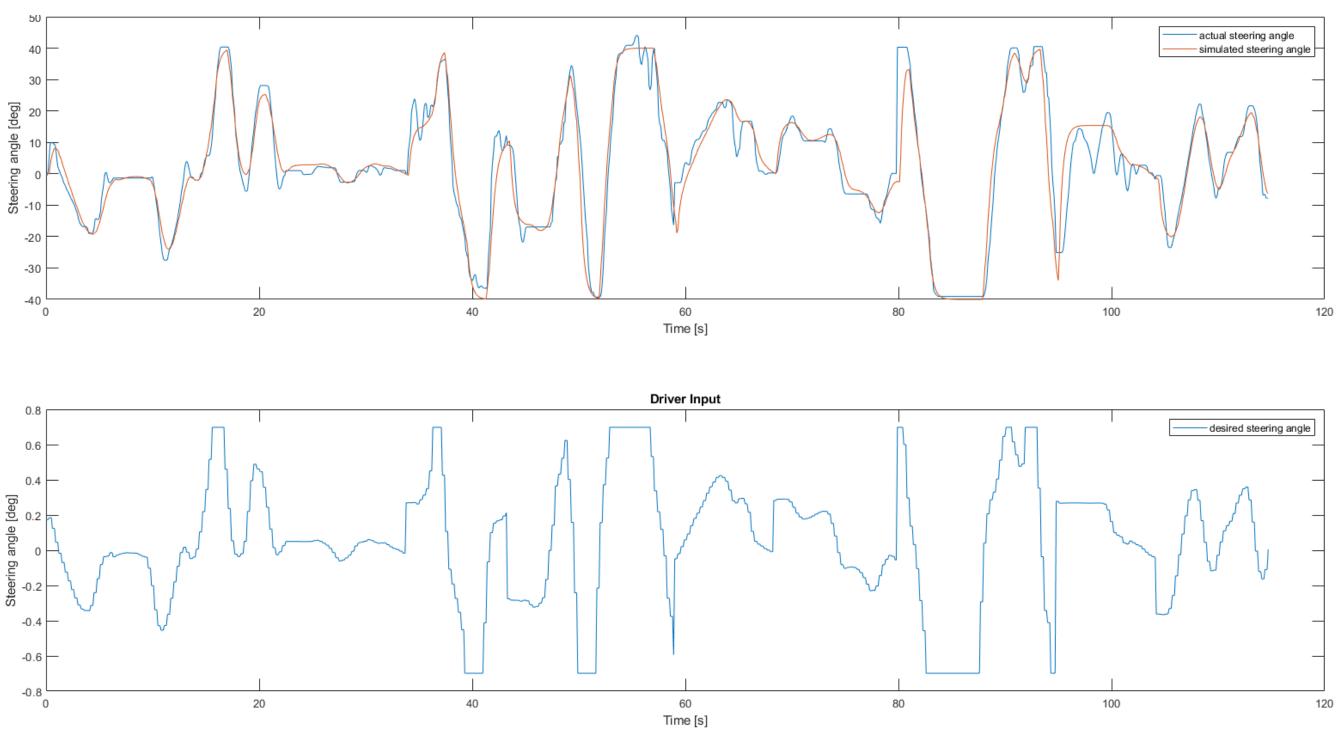
 $\tau =$ Reaction time delay $T_N =$ Neuromuscular lag K, T_L and T_l Adjustable by driver depending on controlled system

the driver constants



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•System identification (Interior-point optimization algorithm) used to determine

Cost Function Definition

- Reference path tracking
- Reference velocity tracking
- Steer rate suppression

$$J_{y}(\mathbf{x}(k)) = \left(w_{\mathbf{y}}[x_{1,\mathrm{ref}}(k) - x_{1}(k)]\right)^{2} + \left(w_{\mathbf{y}}[y_{1,\mathrm{ref}}(k) - y_{1}(k)]\right)^{2}$$
$$J_{u}(\mathbf{u}(k)) = \left(w_{v_{0}}[v_{0,\mathrm{ref}}(k) - v_{0}(k)]\right)^{2}$$
$$J_{\Delta u}(\mathbf{u}(k)) = \left(w_{\Delta\delta}[\delta_{\mathrm{d}}(k) - \delta_{\mathrm{d}}(k - 1)]\right)^{2}$$

e

•Weights tuning*

$$J(\mathbf{x}(k), \mathbf{u}(k)) = J_y(\mathbf{x}(k)) + J_u(\mathbf{u}(k)) + J_{\Delta u}(\mathbf{u}(k))$$

*Model Predictive Control-based Driver Assistance System | TU Delft Repositories



$$\sum_{k=0}^{N} J(\mathbf{x}(k), \mathbf{u}(k))$$

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Controller Implementation and Verification

- Model in the Loop (Without driver interaction) Matlab environment
- •Hardware in the loop Experimental testing
- •Human in the loop Virtual Reality Simulator







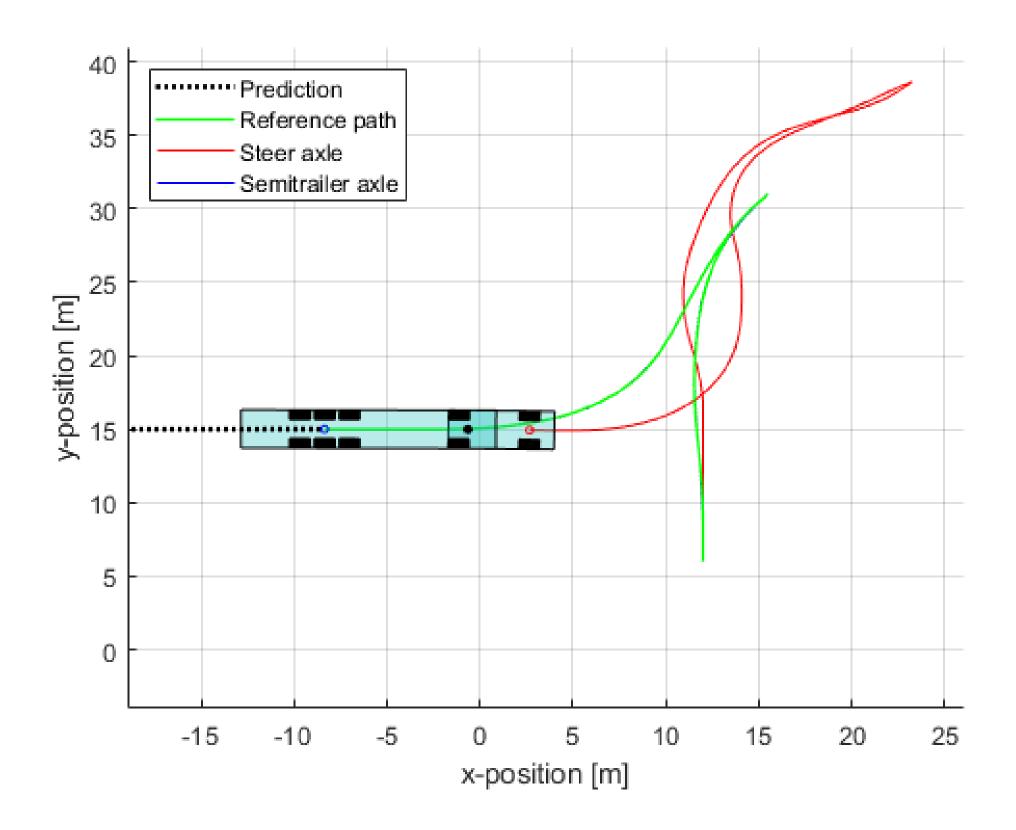
teraction) – Matlab environment I testing imulator



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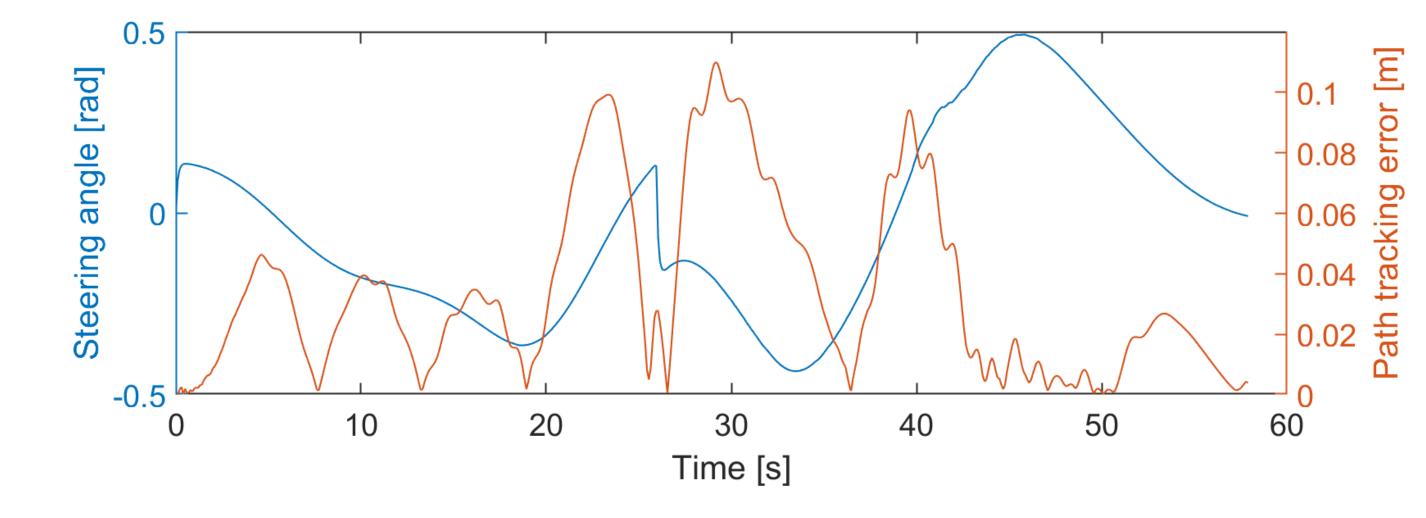
Model in the Loop

- •Driver is assumed as perfect actuator (i.e. no delays or disturbances)





•Vehicle behaviour and its model representation in MPC framework is consistent





AVEC'22 Hardware in the Loop (Scaled vehicle platform)

- •Verification of robustness
- Vehicle combination experiences tyre slip
- •Unequal load distribution (combination weight 290 kg)
- •Remotely controllable w.r.t. steering and drive torque
- Localization of each unit by RTK GPS







Hardware in the Loop – Autonomous docking



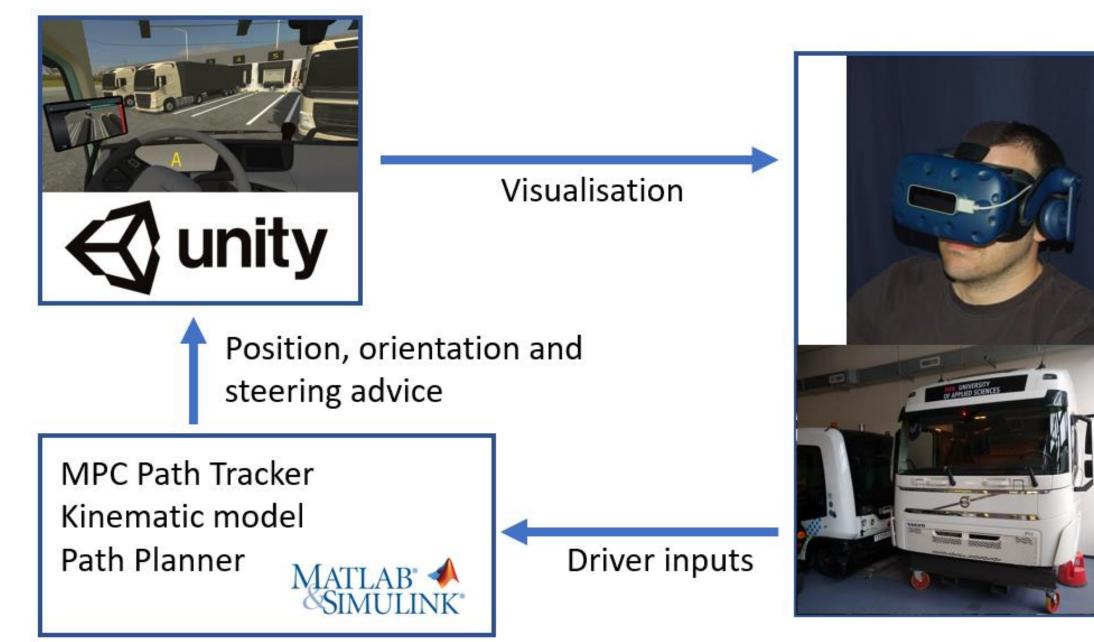


Human in the Loop @ Virtual Reality Simulator*

- •Verification of robustness with Human drivers in the Loop
- •Test various HMI setups
- •Examine the drivers acceptance (w.r.t. HMI, reference paths)
- Test failure scenarios

* Applied Sciences | Free Full-Text | A VR Truck Docking Simulator Platform for Developing Personalized Driver Assistance (mdpi.com)

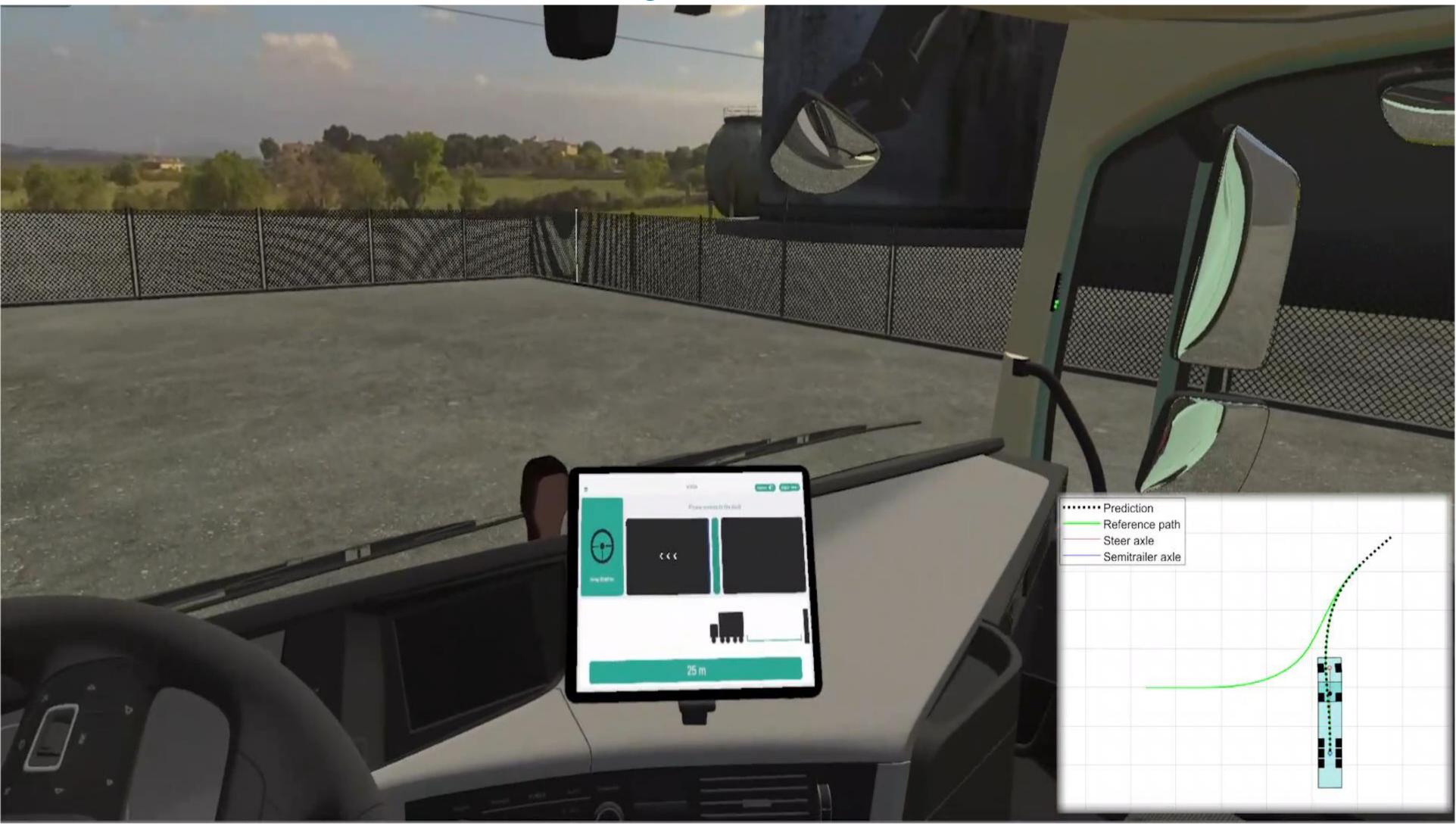








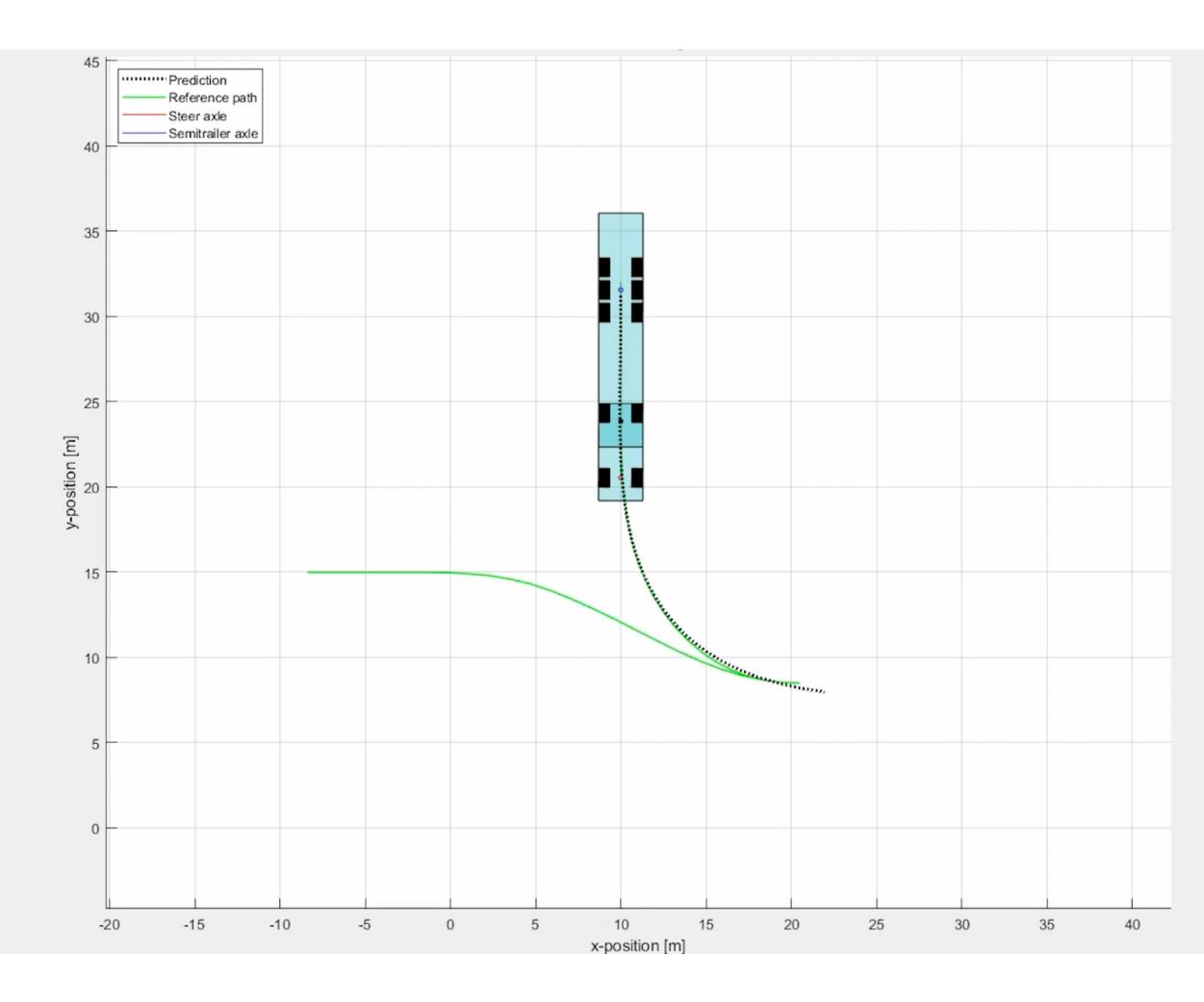
Virtual Reality Simulator View



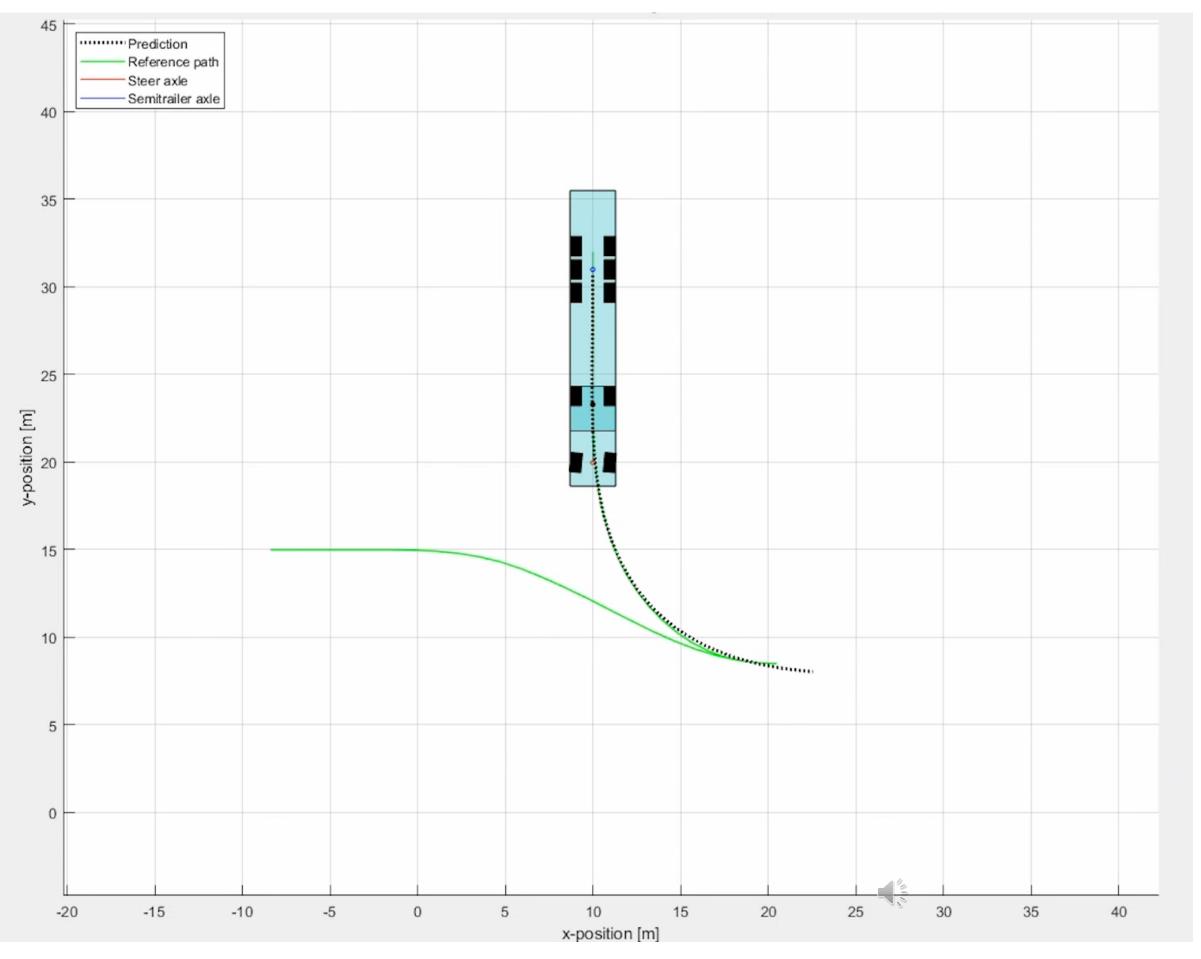


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Docking without Assistance



AVEC'22 Docking with Assistance





Conclusions

- MPC-based bidirectional path tracking controller appears as promising solution for both:
 - Automated docking of articulated vehicles
 Assisted (driver in the loop) docking of articulated vehicles
- The method proves sufficiently robust when deployed into physical scaled demonstrator and even though a considerably simplified model of the vehicle behaviour is used.
- The controller appeared to be more forgiving to driver-introduced steering angle deviations and delays compared to previously developed controllers, i.e. desired steering angle dynamics were perceived as more naturalistic.





Research outlook – installing the entire VISTA framework on pilot site and testing in real life conditions







Research outlook – MPC-Based Full Scale Autodocking





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THANK YOU

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